

Description

Control input circuit for an electrical appliance

The invention relates to a control input circuit for an electrical appliance. A control input is an electrical interface for an appliance, which interface can be used to send electronic control signals from an external control unit to the appliance provided with the control input. Such control signals include turn-on and turn-off commands, for example. The appliance provided with the control input is any electrical appliance which is able to detect and process electronic control signals, particularly an electric motor unit, a measurement appliance, a data recording or reproduction appliance or the like. A control unit may be a programmable logic controller (PLC), in particular.

The control signal is produced by applying a control voltage to the control input of the appliance. In this context, the control input circuit associated with the control input has the task of recording the control current excited by the control voltage and, if a control signal is present, triggering an appropriate reaction to the control signal in the appliance.

Various control voltages are usual which differ in terms of voltage level and voltage form, particularly DC or AC voltage. In particular, the use of 24 V DC, 48 V DC, 110 V AC, 230 V AC etc. as control voltage is customary. In line with conventional nomenclature, DC stands for DC voltage and AC stands for AC voltage in this context.

To increase the compatibility of an appliance, and at the same time to have to provide the smallest possible number of different control inputs, it is usual practice to design a control input for a bandwidth comprising a plurality of control

voltages, e.g. for 24 V DC to 48 V DC or 110 V AC to 230 V AC. In this connection, it would be desirable to have a control input which is equally suitable for all common voltage levels and also for DC and AC voltages.

A conventional control input circuit with a purely nonreactive input characteristic can generally fulfill this not at all or only inadequately, especially since a rising control voltage usually means that it is also necessary to take account of a rising residual current which inevitably flows through the control line connecting the appliance to the control unit even when there is currently no control signal applied. In addition, this residual current is overlaid by interference currents which are transferred to the control line, particularly through capacitive interference injection. Such interference injection may arise, by way of example, when the control line is placed close to a network cable with only inadequate shielding. A control input circuit designed for wideband control voltages must imperatively have a comparatively low trigger threshold in order to trigger with certainty when a low control voltage is used. On the other hand, however, this means that a control input circuit with a nonreactive characteristic has an increased risk of the trigger threshold being exceeded merely on account of the residual current and/or the interference current when a high control voltage is used.

To increase the wide bandwidth of a control input, from time to time a control input circuit is also used which contains a constant current sink. The term constant current sink is understood to mean a circuit module whose drawn current is largely independent of the applied voltage within a prescribed voltage range. In the case of a control input circuit of the latter type, however, it is usually possible to set only a comparatively small drawn current in order to limit the maximum

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power loss arising in the control input circuit and the
associated heating of the appliance to a tenable

degree. The maximum drawn current which can be set without the need to provide complex overheating protection is in this case often too small to reach the minimum turned-on current demanded in accordance with the relevant standards, e.g. EN 61131-2: 1994.

The invention is based on the object of specifying a control input circuit for an electrical appliance whose voltage level and voltage form is suitable for a particularly large bandwidth of control voltages. In particular, the control input circuit in this case needs to be insensitive toward a capacitive interference current and needs to have low electrical loss. The invention is also based on the object of specifying an electrical appliance with an improved control input.

The invention achieves the object for the control input circuit by means of the features of claim 1. The control input circuit accordingly comprises a constant current sink with pulsed operation in terms of its drawn current. In this context, the drawn current assumes a detection value during the length of a detection pulse. Between two respective detection pulses at successive times, the drawn current is lowered in comparison with this detection value. To identify an applied control signal, the control input circuit also comprises an evaluation module. This is designed such that a control signal is indicated, i.e. particularly an internal appliance controller in the appliance is able to recognize when during the detection pulse the control current is not below a prescribed turned-on value for a prescribed turned-on period.

With regard to the appliance, the invention achieves the object by means of the features of claim 18. The control input of the appliance accordingly has the inventive control input circuit associated with it.

The pulsed operation of the constant current sink reduces the average power loss arising at the control input to a comparatively low level, especially since the constant current sink permits an increased flow of current, and hence a significant power loss, only during the detection pulses. In a quiescent phase between two respective successive detection pulses, the drawn current is by contrast reduced to a low level, which means that only a low power loss arises during the quiescent phase. The heat loss which has arisen during the preceding detection pulse is therefore dissipated to a sufficient extent during the quiescent phase with just simple means, in order to prevent the appliance from overheating. This in turn allows the drawn current during a detection pulse to be chosen to be particularly large, which lowers the control input circuit's susceptibility to interference from interference currents. With an evaluation module which indicates the presence of a control signal only if during the prescribed turned-on time the control current is not below a prescribed turned-on value, interference influences can be masked out. The turned-on value is advantageously chosen to be slightly lower than the detection value of the drawn current, but high in comparison with the drawn current of the constant current sink during the quiescent phase. The turned-on period is in the order of magnitude of the detection pulse, but is preferably chosen to be somewhat shorter than the latter, in order to intercept edge rise times for the input voltage and the like.

To actuate the constant current sink, i.e. to prescribe the absolute value of the drawn current, it preferably has an actuation module connected to it. This is advantageously produced by an oscillator circuit whose total resistance alternates discretely between two values. Such a discrete oscillator circuit is also called an astable multivibrator (see U. Tietze, Ch. Schenk, Halbleiterschaltungstechnik [Semiconductor circuitry], 11th edition, Section 6.2.3, p. 603,

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1999, Berlin (Springer Verlag)). In a compact alternative which is favorable in terms of the complexity of parts, the

actuation module provided is a microprocessor. This microprocessor expediently also performs other control functions for the appliance in addition to actuating the constant current sink.

In one preferred embodiment, the constant current sink has a diode connected upstream of it. This enhances the control input circuit in particularly simple fashion to pick up both DC voltage and AC voltage. With regard to the use of an AC voltage as control voltage, the additional advantage arises that the rectifying effect of the diode means that the control input circuit needs to be designed only for one voltage polarity. In addition, a current flows through the constant current sink only during that half-cycle of the control voltage whose polarity is in the forward direction of the diode, which assists in further reducing the power loss arising in the control input.

The evaluation module is particularly easily formed by an RC element which is charged when a control signal is applied. In this context, the RC element is proportioned such that the output voltage present across the RC element reaches a trigger value as soon as the control current is not below the prescribed turned-on value during the prescribed turned-on period. To mask out interference influences with certainty, the RC element advantageously has a threshold circuit connected upstream of it which is turned on only when the absolute value of the input current flowing in the control line exceeds a turned-on value.

In one simple and effective embodiment, the constant current sink is formed by a field effect transistor (FET) whose gate connection is placed at a constant voltage.

Preferably, the detection pulses are periodically successive in time. When a DC voltage is used as the control voltage,

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the period length is firmly prescribed by the actuation module
in this

case. When an AC voltage is used as the control voltage, on the other hand, the actuation module expediently coordinates (or synchronizes) the period of the detection pulses with the phase of the control voltage. In this context, the detection pulses are thus "triggered" by the control voltage, which means that the profile of the control voltage is always the same during the length of an arbitrary detection pulse. In particular, the actuation module is in a form such that the start of a detection pulse always coincides with the start of a positive half cycle of the control voltage. As a result, particularly low power loss arises, especially with a sinusoidal control voltage.

With a particularly advantageous design for the control input circuit with regard to common control voltages, i.e. particularly 24 V - 230 V AC/DC, the drawn current of the constant current sink between two successive detection pulses is lowered by at least a factor of 10, particularly at least a factor of 20, in comparison with the detection value, whereas the turned-on value of the evaluation module is fixed at approximately 85% of the detection value. In this context, the detection value is approximately 8 mA, in particular. The prescribed turned-on period, during which the input current needs to exceed the turned-on value in order to trigger a control operation, is at least 70%, preferably approximately 90% of the length of a detection pulse. In addition, the period of time between two successive detection pulses, i.e. the length of the quiescent phase, exceeds the length of a detection pulse by at least twofold. In particular, the length of the quiescent phase is approximately four times the length of a detection pulse. In this case, the length of a detection pulse is approximately 4 ms, in particular.

The numerical values and relations listed in the previous paragraph may also be used individually and in any combination as advantageous embodiments of the invention.

To attain a compact design for the control input circuit and low complexity of parts, the control input circuit or portions thereof are preferably in the form of an integrated circuit (ASIC).

The inventive control input circuit can be used particularly advantageously in an electrical appliance which can be actuated by electronic control signals. The use of the control input circuit in the appliance ensures a particularly high level of compatibility with various control units. The appliance equipped with the inventive control input circuit can be addressed particularly using all common control voltages, e.g. 24 V - 230 V AC/DC, without requiring any specific adaptation of the control input. In this context, only a comparatively low power loss arises in the control input on average over time, even with a high control voltage, which means that no complex precautions for dissipating the heat loss are required. This allows inexpensive and compact implementation of the appliance.

Exemplary embodiments of the invention are explained in more detail below with reference to a drawing, in which:

FIGURE 1 schematically shows a switching arrangement with an electrical appliance and a control unit addressing the appliance via a control line,

FIGURE 2 shows a schematic diagram of the time profile of the control voltage and of the input current flowing in the control line during a control signal when a sinusoidal control voltage is used,

FIGURE 3 uses an illustration based on FIGURE 2 to show the control voltage and the input current during a control signal with a control voltage which is constant over time,

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FIGURE 4 shows an electronic circuit diagram of a control input circuit in the appliance, and

FIGURE 5 shows an electronic circuit diagram of an alternative embodiment of the control input circuit.

Mutually corresponding parts and variables are always provided with the same reference symbol in the figures.

FIGURE 1 shows a coarsely schematic simplification of a switching arrangement with an electrical appliance 1 to which electronic control signals S are supplied from an external control unit 3 via a control line 2. The appliance 1 is an electronic motor unit, for example. The control unit 3 is a programmable logic controller, particularly a computer, for example.

The control unit 3 is for its part supplied with power by means of a mains line 4 carrying a mains voltage U_n .

To produce a control signal S , the control unit 3 applies a control voltage U_{st} to a control input 5 of the appliance 1. With respect to the control line 2, the control input 5 forms the interface between the appliance 1 and the appliance exterior. The control voltage U_{st} used is either a DC voltage or an AC voltage. In this context, the absolute value of the voltage or the voltage amplitude of the control voltage U_{st} is normally chosen to be between 24 V and 230 V, depending on the design of the control unit 3. The control voltage U_{st} is present across a control input circuit 6 connected into the control line 2 within the appliance 1. The control input circuit 6 analyzes the voltage which is present in the control line 2 and, when a control signal S is applied, actuates an internal appliance controller (not shown in more detail) as appropriate. The control signal S is a turn-on or turn-off command, for example. In this case, the appliance 1 is turned on or turned off when a control voltage U_{st} is applied.

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When a control signal S is present, the control input circuit 6 has a comparatively large input current I_e flowing through it

under the action of the applied control voltage U_{st} . When the control line 2 is not activated, i.e. in the absence of a control signal S , the absolute value of the input current I_e is by contrast reduced to a low level. However, the input current I_e generally assumes an absolute value which is significantly different than zero even when a control signal S is absent. The reason for this is firstly a residual current I_r which inevitably appears within the control unit 3 and which secondly has an interference current I_s overlaid on it. The interference current I_s is injected into the control line 2 in predominantly capacitive fashion. This occurs, by way of example, as a result of the control line 2 being laid adjacent to the mains line 4, if the latter is not sufficiently well shielded. The coupling capacitance C_k between the control line 2 and the mains line 4 is indicated in the diagram shown in FIGURE 1 by an equivalent circuit diagram in the form of a capacitor.

The control input circuit 6 comprises a constant current sink 7 connected into the control line 2 (FIGURE 4). The constant current sink 7 holds the absolute value of the input current I_e at a constant absolute value, i.e. an absolute value which is essentially independent of the control voltage U_{st} , if this absolute value denoted as drawn current I_a is provided. The constant current sink 7 is operated in pulsed mode. In other words, the drawn current I_a is a function of time whose magnitude varies in pulsed fashion.

In practice, the constant current sink 7 has a comparatively high drawn current I_a during periodically recurring detection pulses P (FIGURES 2 and 3). During a detection pulse P which has a length t_1 of 4 ms, for example, the drawn current I_a assumes a comparatively large value of approximately 8 mA, which is subsequently called detection value I_1 . The period of time between two successive detection pulses P is called quiescent phase R . During this quiescent phase R , the drawn current I_a of

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the constant current sink 7 is lowered significantly in
comparison with the

detection value I_1 , for example by a factor of 20, to a quiescent value I_2 . The length t_2 of the quiescent phase R exceeds the length t_1 of the detection pulse P by at least twofold, preferably even fourfold.

If a control signal S is present, a constant input current $I_e = I_1$ flows almost during the entire length of the detection pulse P. During the subsequent quiescent phase R, the flow of current through the control input circuit 6 is limited to the quiescent value I_2 at maximum, so that during the quiescent phase R in the control input circuit 6 only low power loss occurs. The average power loss occurring over time is therefore comparatively low, which effectively reduces the risk of the appliance 1 overheating, particularly in the region of the control input circuit 6.

This is explained in more detail in Figures 2 and 3. Both figures use a timing diagram to show a profile of the control voltage U_{st} during a control signal S in comparison with the corresponding input current I_e .

FIGURE 2 shows the input current I_e which becomes established when using a sinusoidal AC voltage as control voltage U_{st} . The constant current sink 7 synchronizes itself, as described in more detail below, automatically with the phase of the control voltage U_{st} by virtue of a detection pulse P always being started at the start of the positive half cycle of the control voltage U_{st} . In other words, the detection pulses P are respectively "triggered" by the zero crossing of the control voltage U_{st} for the positive half cycle. As FIGURE 2 reveals, the drawn current I_a of the constant current sink 7 is switched down from the detection value I_1 to the comparatively low quiescent value I_2 after the detection pulse P, with the timing of the subsequent quiescent phase R extending at least over the entire residual length of the positive half cycle of the

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control voltage U_{st} . The absolute value of the input current I_e during the

entire positive half cycle of the control voltage U_{st} corresponds to the drawn current I_a .

The control voltage U_{st} is rectified within the control input circuit 6, so that the flow of current in the control line 2 comes to a standstill during the negative half cycle of the control voltage U_{st} .

FIGURE 3 shows the input current I_e , as becomes established for a control voltage U_{st} which is constant over time. In this case, the period of the recurring detection pulse P is prescribed internally by the control input circuit 6. A period comprises a detection pulse P of length t_1 which is followed by a quiescent phase R of length t_2 .

While there is no control signal S applied to the control input 5, the input current I_e is necessarily equal to the sum of the residual current I_r and the interference current I_s . This sum $I_r + I_s$ is generally small around the detection value I_1 and fluctuates irregularly. During a detection pulse P , the input current I_e is therefore generally below the drawn current $I_a = I_1$ prescribed by the constant current sink 7. This value is reached for a short time at the outside, e.g. when a high interference voltage is briefly injected on account of a switching operation in the mains line 4 which provides coupling to the control line 2. The input current I_e can then reach the detection value I_1 at most. However, the length of such interference influences is generally short around the length t_1 of a detection pulse P , so that the input current I_e flowing on average over time during the detection pulse P continues to be small in comparison with the correspondingly averaged input current I_e which flows during a control signal S .

By evaluating the input current I_e flowing during a detection pulse P , it is thus possible to distinguish a control signal S

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more or less clearly from interference influences. This principle for identifying a control signal S is

implemented in the control input circuit 6 described in detail below.

An exemplary embodiment of the control input circuit 6 is shown in FIGURE 4 in an electronic circuit diagram. The constant current sink 7 connected into the control line 2 accordingly has a diode D1 connected upstream of it for the purpose of rectifying the control voltage U_{st} .

The constant current sink 7 comprises a field effect transistor T1 whose drain connection 8 is connected to an input contact 9 of the control input 5. The drain connection 8 is connected via a resistor R1 to the gate connection 10 of the field effect transistor T1, which is in turn connected via a Zener diode ZD1 oriented in the reverse direction to an output contact 11 of the control input 5. In this circuitry, the gate connection 10 of the field effect transistor T1 has a constant voltage applied to it which fixes the input current I_e flowing through the field effect transistor T1 between the drain connection 8 and the source connection 12 at a constant value, i.e. the drawn current I_a .

The magnitude of the drawn current I_a is calculated from the breakdown voltage of the Zener diode ZD1 divided by the total resistance R_S between the source connection 12 of the field effect transistor T1 and the output contact 11. To influence this total resistance R_S , the source of the field effect transistor T1 has an actuation module 13 connected downstream of it.

The actuation module 13 comprises three transistors T2, T3 and T5 which have connected resistors R2, R3, R4, R5, R6, R7, R8, R9, R13, R14 and R15, a diode D2 and a capacitor C1 as shown in FIGURE 4.

The transistors T2, T3 and T5 are connected up such that during the detection pulse P only the transistor T3 is on, i.e. has a conducting collector/emitter

path. In this context, the total resistance R_S is essentially provided by the series circuit comprising the resistors R_8 and R_9 . The detection value I_1 of the drawn current I_a is thus essentially obtained from the breakdown voltage of the Zener diode $DC1$ divided by $R_8 + R_9$.

In the quiescent phase R , on the other hand, the transistors T_2 and T_5 are on. The total resistance R_S is then obtained approximately from the parallel circuit comprising the resistors R_{15} and R_5 . The quiescent value I_2 of the drawn current I_a is thus provided approximately by the breakdown voltage of the Zener diode $DZ1$ divided by $R_{15} \cdot R_5 / (R_{15} + R_5)$. Suitable circuit design achieves a situation in which the quiescent value I_2 of the drawn current I_a is significantly smaller than the detection value I_1 . The length t_1 of the detection pulse P and the length t_2 of the quiescent phase R can be set independently of one another by stipulating the dimensions of the capacitor C_1 and of the resistors R_2 and R_3 .

When an AC voltage is used as control voltage U_{st} , the actuation module 13 restarts at the beginning of every positive half cycle. This is done by virtue of the RC element 14 formed by the resistor R_3 and the capacitor C_1 being charged via the resistor R_{15} , the resistor R_2 and the diode D_2 . In this context, the base voltage of the transistor T_2 connected to the RC element 14 via the resistor R_4 rises until said transistor is turned on after the length t_1 . This terminates the detection pulse P . The transistor T_3 , which had been on when the actuation module 13 started, is turned off by the transistor T_2 which is turned on, and the transistor T_5 which was off during the detection pulse P is in turn turned on when the transistor T_3 is turned off. This shorts the output side of the resistor R_{15} to the output contact 11. The RC element 14 is now not charged any more, but rather discharges gradually via the resistor R_3 .

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During the negative half cycle of the control voltage U_{st} , the flow of current breaks down. This causes the RC element to discharge

completely. At the start of the next positive half cycle of the control voltage U_{st} , the process described above is repeated again.

With a constant control voltage U_{st} , the actuation module 13 oscillates periodically with the prescribed pulse/pause ratio between the detection pulse P and the quiescent phase R.

The actuation module 13 has an evaluation module 15 connected in parallel with it. The evaluation module 15 comprises an RC element 16 which is connected between the source output 12 of the field effect transistor T1 and the output contact 11 and which is formed from a resistor R12 and a capacitor C2. Connected between the field effect transistor T1 and the RC element 16 is a threshold circuit 17 which opens the connection between the RC element 16 and the field effect transistor T1 when the input current I_e exceeds a prescribed turned-on value. To this end, the threshold circuit 17 uses a voltage divider circuit containing the resistors R10 and R11 and also a Zener diode ZD2 oriented in the reverse direction to pick off the voltage across the resistor R8 through which current flows during the detection pulse P. The threshold circuit 17 also comprises a transistor T4 whose base is connected to the output potential of the resistor R11. The transistor T4 is turned on when the breakdown voltage of the Zener diode ZD2 is present across the resistor R8, and consequently current flows through the resistors R10, R11 and the Zener diode ZD2. The voltage which is present across the resistor R8 is proportional to the input current I_e flowing through the resistor R8. The breakdown voltage of the Zener diode ZD2 is in this case chosen such that the transistor T4 is turned on when the input current I_e corresponds to the turned-on value of approximately 85% of the detection value I_1 .

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When the transistor T4 is on, the RC element 16 is charged. As a result, the voltage which is present across the RC element 16 and which can be picked off at contacts 18 and 19

as output voltage U_a rises gradually during the detection pulse P .

During the quiescent phase R , the input current I_e corresponds at most to the quiescent value I_2 of the drawn current I_a . This quiescent value I_2 is significantly below the turned-on value, which means that further charging of the RC element 16 is prevented. The RC element 16 is consequently discharged via the resistor R_{12} during the quiescent phase R .

In the case of the present control signal S , the transistor T_4 is for the largest part turned on during a detection pulse P . The output voltage U_a consequently reaches a comparatively high value at the end of the detection pulse P , said high value reaching a prescribed trigger threshold if the input current I_e is not below the turned-on value during a prescribed turned-on period. The turned-on period is chosen to be slightly shorter than the length t_1 of the detection pulse P , in order to cushion edge rise times for the input current and the like. Preferably, the turned-on period is approximately 90% of the length t_1 .

The fact that the output voltage U_a reaches or exceeds the trigger threshold means that, again in a manner which is not shown in more detail, an internal appliance controller in the appliance 1, which appliance controller is connected to the contacts 18 and 19, recognizes the presence of the control signal S and triggers a reaction from the appliance 1 which is based on the control signal S .

If there is no control signal S present, the transistor T_4 remains for the largest part turned off during the detection pulse P . The RC element 16 is thus largely not charged. As a result, the output voltage U_a remains at a very low value which is constantly below the trigger threshold, in particular.

In an alternative exemplary embodiment of the control input circuit 6 shown in FIGURE 5, a subfunction of the actuation module 13 is implemented in a microprocessor 20. The microprocessor 20 has a fraction of the rectified control voltage U_{st} across a voltage divider comprising resistors R16 and R17 supplied to it via a voltage input 21. The microprocessor 20 also has a control output 22 which it uses to actuate the transistor T3 on the basis of the control voltage U_{st} . In a similar fashion to the exemplary embodiment shown in FIGURE 4, the transistor T3 is connected in series with the resistor R8 between the source connection 12 of the field effect transistor T1 and the output contact 11 of the control input 5. The transistor T3 is actuated by the microprocessor 20 such that a time profile for the input current I_e as shown in FIGURES 2 and 3 is obtained.

The input current I_e is analyzed by the evaluation module 15, whose design and manner of operation are unaltered in comparison with FIGURE 4. However, the output voltage U_a is supplied to a trigger input 23 of the microprocessor 20. In this context, the microprocessor 20 simultaneously undertakes the function of an internal appliance controller and in this function actuates the appliance 1 in appropriate fashion when the output voltage U_a exceeds the prescribed trigger threshold.

The use of the term "module" for the functional groups of the control input circuit 6, particularly the actuation module 13 and the evaluation module 15, does not necessarily imply any physical separation of these groups. Rather, the entire control input circuit 6 or arbitrary parts thereof are preferably arranged in an arbitrary physical arrangement on a common circuit support. The control input circuit 6 or parts thereof are preferably in the form of an integrated circuit (ASIC).